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Synthesis of new ionic liquid-grafted metal-oxo nanoclusters – Design of nanostructured hybrid organic-inorganic polymer networks

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ABSTRACT

Designing innovative multi-functional thermoset polymers represents a major challenge in materials science. In this work, two novel polyhedral imidazolium ionic liquid supported on oligomeric silsesquioxane nanocages having chloride (Cl⁻) and bistrifluoromethanesulfonimidate (NTf₂) counter anions have been synthesized. These ionic nano-objects were used to nanostructure a model epoxy network. Hence, networks displaying a homogeneous nanoscale morphology were obtained by introducing 5 wt % of such organic-inorganic (O/I) silicon-oxo clusters functionalized with ionic liquids. The obtained ionic hybrid O/I epoxy-amine networks display an excellent thermal stability (>400 °C) compared to their neat counterparts, as well as a pronounced hydrophobic character (23 mJ m⁻²) and good mechanical performances. Moreover, these O/I nanostructured networks demonstrate an improved fire resistance according to pyrolysis-combustion flow calorimetry (PCFC) and cone calorimetry analyses. In fact, the use of low amounts of inidazolium ionic liquid-modified polyhedral oligomeric silsesquioxanes induce a significant decrease of heat release rate (about 55%), as well as a retardation of the ignition time (close to 29%) compared to the neat epoxy-amine network.

Keywords: Ionic liquid Polyhedral oligomeric silsesquioxane (POSS®) Epoxy network Organic-inorganic nanomaterials Fire resistance

1. Introduction

Due to their interesting physical properties including optical transparency, high electrical resistance and thermal insulation capabilities in parallel with good thermo-mechanical properties and dimensional stability, epoxy networks represent an important class of thermoset polymers, widely used in applications going from adhesives, paints and coatings, insulating layers in electronics to matrices for composites used in automotive and aerospace industries [1,2]. However, the highly-crosslinked nature of such thermoset polymers leads to a brittle behavior, *i.e.* materials with a poor resistance to crack propagation when subjected to mechanical loading, as well as thermal changes [3,4]. More particularly, the fire resistance of epoxy polymers based on diglycidyl ether of bisphenol A (DGEBA) is a major drawback restricting their use for applications requiring high-standard fire safety [5,6].

In order to overcome these limitations, various routes have been investigated over the years. Regarding improvement of toughness, the most common approach consists in introducing a dispersed ductile phase within the epoxy network using thermally stable and high-T $_{\rm g}$ thermoplastic polymers (TP) (such as polyetherimide (PEI), polyethersulfone (PES), polyphenylene ether (PPE)) or reactive elastomers (such as functionalized poly(butadiene-co-acrylonitrile) rubbers (CTBN, ETBN)) through a reaction-induced phase separation occurring during curing [7–9]. Nevertheless, the incorporation of such compounds usually results in a significant reduction of stiffness (*i.e.* Young modulus) and in some cases to a lower glass transition temperature due to non-perfect microphase separation, in addition to an important increase of flammability.

Regarding fire resistance, two main approaches have been studied to obtain fire resistant (FR) epoxy polymers: the first consists in introducing halogenated fire-retardant compounds in a conventional epoxy polymer, and the second involves modifying the chemical structure of the epoxy prepolymer (*e.g.* brominated epoxy resins). Nowadays, such compounds tend to be subjected to drastic regulations, in terms of quantity and field of use, due to environmental and health concerns regulated by new European directives such as REACH [10]. Research

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groups have thus been looking for alternatives, among which phosphorus-based compounds, phosphorus-modified resin backbones and/or hardeners have attracted great interest [11]. In many cases though, those compounds need to be used in high concentration, which can sometimes bring detrimental changes to other material properties such as mechanical properties [12]. More recently, others improvement routes reported in the literature have turned towards the introduction of nanoparticles, such as silicate clays or carbon nanotubes, in order to combine the effects of reinforcement of filled polymers and the fire resistance conveyed by nanocomposites [13,14]. Nonetheless, such synergetic effect can only be obtained if the nanoparticles are well dispersed, which remains challenging and rather difficult for most polymers. Referring to recent studies, a promising path seems to be the introduction of polyhedral oligomeric silsesquioxane (POSS®), known for their fire-retardant properties, into epoxy networks [13,15,16].

Polyhedral Oligomeric Silsesquioxanes, now called POSS®, refer to all the molecular structures with the empirical formula $(RSiO_{1,5})_n$, where R is a hydrogen atom or an organofunctional derivative of alkyl, alkylene aryl, or arylene groups. The terme "silesqui" refers to the ratio of the silicon to oxygen atoms, *i.e.* Si:O = 1:1.5 [17]. POSS® are incompletely oxidized silicate compound compared to SiO₂ with a cage structure having different numbers of silicon atoms. The sizes of these molecular objects range from 1 to 3 nm [17]. The most common POSS® have a cubic T₈ cages with a general formula R₈Si₈O₁₂ [17]. Numerous papers reported studies on hybrid organic-inorganic (O/I) nanomaterials based on epoxy matrices modified by POSS®. For example, Laine et al. [18-22] and Matejka et al. [23] described the effect of a series of functionalized and non-functionalized POSS® with various R groups such as aminophenyl, dimethylsiloxypropylglycidyl ether, epoxy, or alkyl groups (isobutyl, methyl, and ethyl) on the dynamic mechanical properties, fracture toughness, and thermal stability of the resulting O/I epoxy nanomaterials. The incorporation of POSS® in epoxy networks can result both in an increase [24-26] or a decrease [27, 28] of mechanical properties, *i.e.* stiffness and toughness. In fact, POSS® nano-objects usually tend to easily aggregate leading to the formation of inorganic-rich domains within the epoxy networks [23]. Therefore, tailoring the balance of interactions between the polymer medium, the O/I nanoparticles and the POSS®-POSS® interaction (leading to the formation of microsize aggregates) is a key issue for designing proper inorganic-rich nanostructures required for enhancements of mechanical properties [29-36] in addition to fire resistance. Recently, several groups reported significant advantages of using ionic liquids (ILs) as dispersing agents for epoxy matrices reinforced with silica nanoparticles [37,38]. These authors have shown that the introduction of ILs based on imidazolium-based cations was a promising strategy for tailoring nanocomposite morphology at the nanoscale [37,38].

ILs are organic salts with a melting temperature lower than 100 °C that were recently proposed to be combined with epoxy curing chemistry to prepare novel functional materials [39-41]. These ionic compounds have interesting properties such as high thermal and chemical stabilities, a low saturation vapor pressure, non-flammability and dispersant capabilities, catalytic activity, and a high ionic conductivity, which makes them very attractive not only for the present purpose but for polymer science in general [42-51]. Hence, ILs have now emerged in many polymer-based applications. For instance, in epoxy chemistry, ILs can act as catalysts and/or curing agents promoting an anionic polymerization of the epoxy prepolymer leading to significant improvements of the thermo-mechanical properties of the resulting networks compared to conventional epoxy networks [52-54]. POSS® and ionic liquids have also been recently combined to prepare new hybrid compounds by synthesizing IL-grafted POSS®. The corresponding ionic O/I nanoclusters have been used as electrolytes for electrochemical devices [55] or to enhance the proton conductivity of membranes [56] but to the best of our knowledge no authors have proposed to introduce such nano-objects in an epoxy network. In a previous study, we reported that the connection of ion pairs to POSS® nanoclusters, i.e. from grafting an

ionic liquid of POSS® bearing different organic ligands (isobutyl or phenyl), can significantly improve the POSS®/epoxy matrix interactions and promote the formation of well-dispersed POSS® nanodomains [57]. From these first promising results, we investigate here ionic liquid grafted on phenyl POSS®, denoted as IL-g-POSS®^{Ph} with two different anions (Cl⁻ and NTf₂) considered as hybrid O/I nano-objects for designing nanostructured and multifunctional epoxy-amine networks. The anionic exchange of Cl⁻ to NTf₂ was studied here because the later one is known to give materials with better thermal stability and higher T_g [54,58]. The present study unfolds as following: first, the influence of non-modified POSS®^{Ph} (POSS®^{Ph}-triol) and IL-g-POSS®^{Ph} on the polymerization of the epoxy prepolymer is described. Then, the morphologies of the two types of POSS®^{Ph} modified epoxy networks are compared as well as their physical and mechanical properties. Eventually, the potential for fire retardancy of IL-grafted POSS®^{Ph} modified epoxies is more specifically investigated.

2. Materials and characterization methods

2.1. Materials

1-methylimidazole (99%), 3- chloropropyltrimethoxysilane (97%), isophoronediamine (IPD), and lithium bistrifluoromethanesulfonimidate (LiNTf₂) considered for anionic exchange procedure, the solvents (diethyl ether, ethanol, chloroform, and dichloromethane) were purchased from Sigma Aldrich and used as received. Epoxy prepolymer based on diglycidyl ether of bisphenol A (DGEBA) (EPON 828 from Hexion) and heptaphenyl-trisilanol POSS®, denoted POSS®^{Ph}-triol, from Hybrid Plastics were used as received. All the chemical structures of non-grafted and IL-grafted POSS® used and synthesized are summarized in Table 1.

2.2. Anionic exchange procedure of polyhedral oligomeric silsesquioxane (POSS \mathbb{R}^{Ph}) (chloride Cl^- vs. bistriflimidate NTf_2)

The anion exchange reaction of Cl⁻ by NTf₂ following the same procedure as in Refs. [59,60], *i.e.* an equimolar amount (2.83 g, 9.86 mmol) of LiNTf₂ was added to a solution of IL.Cl-g-POSS®^{Ph} (10 g, 8.96 mmol) in dried ethanol (150 mL) and the mixture was left under stirring at room temperature for 24 h. The resulting white powder was solubilized in dichloromethane (CH₂Cl₂), dried, filtered, and washed several times with water. The obtained product, *i.e.* IL.NTf₂-g-POSS®^{Ph} was then dried at 80 °C for 48 h. The anionic exchange was checked by complexometric chloride titration considering silver nitrate (AgNO₃). The structure of the resulting salts was confirmed by ¹³C NMR and FT-IR spectroscopies as illustrated in Fig. S2 and S3 of the Supporting Information (SI).

2.3. Epoxy network synthesis

Epoxy prepolymer (DGEBA) and isophorone diamine (IPD) were used as co-mononers considering a stoichiometric ratio, *i.e.* amino hydrogen-to-epoxy group equal to one.

5 wt % of POSS®^{Ph}-triol or IL-g-POSS®^{Ph}, either with chloride (Cl⁻) or bis(trifluoromethane)sulfonimide (NTf₂) as counter anions, were incorporated in the epoxy reactive systems. DGEBA and POSS®^{Ph}-triol or IL-g-POSS®^{Ph} were mixed at 120 °C in order to obtain a homogeneous and transparent solution before adding the isophorone diamine used as hardener. Next, the mixture was degassed and then poured into a mold. As a last step, the reactive systems were polymerized for 1 h at 140 °C and post-cured 8 h at 190 °C [61–63] while the epoxy-amine networks with IL-g-POSS®^{Ph} were post-cured a second time at 230 °C for an additional 3 h in order to ensure a complete polymerization.

Table 1

Chemical structures of non-grafted and IL-grafted POSS®.



^a T_m: Melting temperature.

^b T_d: Degradation temperature determined at the maximum of the first derivative of the weight loss as function of the temperature (see Fig. S1 in the SI).

2.4. Sol-gel analysis of hybrid O/I networks

A complete characterization of the POSS®^{Ph}-modified networks is required to determine the amount of POSS®^{Ph} nanocages bonded to the networks. Thus, the POSS®^{Ph}-modified networks were submitted to THF extraction at 60 °C for 24 h to determine a fraction of the soluble portion containing unbounded POSS®^{Ph}. The soluble fraction, denoted as w_s , was evaluated from the weight of the dried specimen, m_{dry} , and the one of the specimen after extraction, $m_{dry-ext}$.

2.5. Characterization

Fourier Transform Infrared Spectroscopy (FTIR): FT-IR spectra were recorded using a Thermo-Scientific Nicolet iS10 Spectrometer from 4000 to 500 cm^{-1} .

 ^{13}C -NMR spectra were recorded using a Bruker Avance II 400 MHz spectrometer at room temperature with appropriate deuterated solvent (acetone-d₆).

Transmission electron microscopy (TEM) was carried out at the Technical Center of Micro-Structures (University of Lyon) using a Phillips CM 120 microscope operating at 80 kV. 60-nm-thick ultrathin sections of samples obtained by ultramicrotomy.

Differential Scanning Calorimetry (DSC) measurements were performed using a DSC Q10 (TA Instruments) in a dynamic mode, *i.e.* with a rate of 10 $^{\circ}$ C min⁻¹ under nitrogen flow (50 mL min⁻¹) from -70 to 300 $^{\circ}$ C.

Dynamic mechanical analyses (DMA) were performed using parallelepipedic specimens ($30 \times 6 \times 3 \text{ mm}^3$) in an ARES-G2 rheometer under torsion mode as a function of temperature with a heating rate of 3 °C min⁻¹. Storage modulus, G', loss modulus, G'', and loss factor, tan δ , were measured from -120 to 250 °C.

Uniaxial compression tests were performed using a MTS 2/M electromechanical testing system at 22 \pm 1 °C and 50 \pm 5 °C relative humidity for a crosshead speed of 1 mm min $^{-1}$ on conventional specimens (5 \times 5 \times 16 mm³). ASTM D695 standard test recommendations were followed. Young's modulus, E, was determined as the slope of the stress-strain curve in the linear domain, *i.e.* at low strain values. Yield strength, σ_y , was taken, as the maximum stress value on stress-strain curve and the strain and stress at break were determined.

Fracture toughness (K_{IC}, G_{IC}).

Fracture properties of neat epoxy-amine and epoxy hybrids O/I networks were determined using compact tension (CT) specimens following the ISO 13586 standard. The primary V notch was machined with a milling machine and the final sharp crack was created by razor tapping at the edge of the main notch.

The critical stress intensity factor K_{IC} is obtained following the standard procedure, while the fracture energy, G_{IC} , in plane stress conditions, was calculated using the following equation (1):

$$G_{IC} = K_{IC}^2 / E (1 - v^2)$$
(1)

where ν is the Poisson's ratio (taken to be 0.35) and E the Young's modulus.

Surface energy of resulting epoxy networks was determined from the sessile drop method using a GBX goniometer. From contact angle measurements measured with water and diiodomethane as probe liquids, polar and dispersive components of surface energy were determined using Owens-Wendt theory [64].

Thermogravimetric analyses (TGA) were performed using a Q500 thermogravimetric analyzer (TA instruments). The samples were heated from 30 to 900 $^{\circ}$ C at 20 $^{\circ}$ C min⁻¹ under air.

Flammability was investigated using a pyrolysis combustion flow calorimeter (PCFC from Fire Testing Technology, UK) initially developed by Lyon and Walters [65]. The sample (3 \pm 0.5 mg) was heated up to 750 °C at 1 °C s⁻¹ in a pyrolyzer under nitrogen flow (anaerobic pyrolysis). The pyrolysis gases were sent to a combustor and mixed with oxygen in excess at 900 °C. In such conditions, these gases were fully oxidized. Heat Release Rate (HRR) was then calculated by oxygen depletion according to Huggett's relation (1 kg of consumed oxygen corresponds to 13.1 MJ of released energy) [66].

Cone calorimeter experiments were performed using a fire Testing Technology equipment, according to the standard ISO 5660 [67]. Square samples of $100 \times 100 \times 30 \text{ mm}^3$ were cut out of larger sheets and their edges polished and wrapped in an aluminum foil leaving only the upper surface apparent to the heater and the lower surface insulated by rock wool. The sample holder was left to cool to room temperature between each test. Every specimen was exposed horizontally under an external heat flow (irradiation) of 35 kW m⁻². Two specimens were tested for each material and the reported data are the average of the two measurements.

Some tests were recorded using an infrared camera (Optris) placed in an inclined position above the specimen in order to record the temperatures of the top surface. The measured temperature depends not only on the surface temperature but also on the tilt of the apparatus relatively to the surface and the emissivity of the materials. Emissivity was chosen equal to 1 (close to conventional values for polymer materials). In these tests, the distance between the radiant cone and the sample was set to 60 mm. Thereby; the tilt of the infrared camera is only of few degrees relative to the perpendicular position, which limits the error of measurements. The uncontrolled expansion of the specimen during burning can also modify this tilt during the test. Finally, the flame can slightly change the measured temperatures. Further description of such device can be found elsewhere [68].

Scanning electron microscopy (SEM) (performed using FEI Quanta 200 ESEM) at an acceleration voltage of 12.5 kV was used to characterize the microstructure of the residual char of samples after the fire test.

Energy Dispersive X-ray spectroscopy (EDX) using Oxford INCA Energy 300 system and a detector of 133 eV was used to determine elemental compositions of residues from the cone calorimeter tests.

3. Results and discussion

3.1. Curing of epoxy-amine and hybrid O/I networks

First, the curing behavior of the epoxy-amine and the different hybrid O/I networks were evaluated with DSC measurements under dynamic mode in order to highlight the impact of IL-g-POSS \mathbb{R}^{Ph} and



Fig. 1. DSC traces of neat epoxy-amine and the hybrid O/I epoxy reactive systems containing 5 wt % $POSS \otimes^{Ph}$ -triol or IL-g- $POSS \otimes^{Ph}$ with Cl^- or NTf_2 anion (heating rate: 10 °C min⁻¹).

POSS®^{Ph}-triol on the reactivity of the polymerization reaction (Fig. 1). As shown in Fig. 1, all the reactive systems, i.e. DGEBA/IPD without and with unmodified or modified POSS®Ph, display an exotherm with a shoulder. According to the literature, such a behavior can be attributed to the adduct formation followed by an addition polymerization [2,40]. Nevertheless, two different behaviors were observed. DGEBA/IPD system with and without POSS®^{Ph}-triol displays the same behavior with an exothermic peak located at 115 °C while DGEBA/IPD containing IL-modified POSS®^{Ph} shows a significant decrease of the temperature of the exothermic peak. This shift of the exothermic peak to lower temperatures can be explained by the presence of imidazolium-based ionic liquid well-known to act as catalytic agents of epoxy-amine networks [54,69,70] hence favoring an early initiation of the polymerization. In addition, a slight increase of the total enthalpy value (ΔH) was observed in presence of IL.Cl-g-POSS®^{Ph} (482.1 J g⁻¹) and IL.NTf₂-g-POSS®^{Ph} (496.5 J g^{-1}) compared to neat epoxy-amine system (460.4 J g^{-1}). Furthermore, the thermograms of hybrid O/I networks containing IL-g-POSS®^{Ph} with different anions show a small additional exothermic peak at higher temperatures (200–250 °C) that can be attributed to the reaction of the imidazolium ionic liquid with epoxy groups [37,54, 70–72]. To confirm this hypothesis, the remaining sol fraction after curing of the different systems was determined. In the case of epoxy networks containing 5 wt % of POSS®^{Ph}-triol, the sol fraction was determined to be 4.8% which means that POSS®^{Ph}-triol clusters are not chemically attached to the epoxy network. For the same amount of IL-grafted POSS®^{Ph}, the sol fraction was found to be 3.4% and 3.6% for IL.Cl-g-POSS®^{Ph} and IL.NTf₂-g-POSS®^{Ph}, respectively. Hence, a covalent grafting of these IL-modified POSS® with the epoxy network is ensured for about 30% of the nanoparticles, while the rest of POSS®^{Ph} remained unbounded. In summary, all these results suggest that the imidazolium ionic liquid grafted to the POSS®^{Ph}-triol with both anions (Cl⁻, NTf₂) acts as an initiator for the ring-opening reaction of the epoxy and a co-curing agent of DGEBA, in agreement with previous studies [37,70].

For all cases, a final epoxy conversion higher than 90% was obtained confirming the good reactivity of DGEBA and IPD comonomers with and without the presence of unmodified or modified POSS®^{Ph} (see Fig. S4). During the 140 °C step, a fast consumption of epoxy functions was observed for epoxy containing IL-g-POSS®^{Ph} (see inlet in Fig. S4) whatever the nature of the anion. At 190 and 230 °C, a progressive consumption of epoxy groups was evidenced confirming the DSC results and highlighting a competition between two polymerization mechanisms, *i.e.* the epoxy-amine condensation reaction and the reaction between IL-g-POSS®^{Ph} and epoxy prepolymer [37].

In conclusion, whatever the anion nature, the reactivity of the imidazolium ionic liquid grafted onto the POSS®^{Ph}-triol nanoclusters towards the epoxy prepolymer (DGEBA) compared to the reactivity of the diamine comonomer (IPD) plays a key role on the kinetics of polymerization, and thus on the architecture of the formed hybrid O/I epoxy networks.

3.2. Morphology of hybrids O/I networks

Transmission electronic microscopy is a powerful tool to highlight the effect of IL-g-POSS®^{Ph} combined with Cl⁻ or NTf₂ on the dispersion of the POSS®^{Ph} nanoclusters into epoxy networks. The morphologies obtained for the different epoxy hybrid O/I networks and the distributions of the POSS®^{Ph}-rich dispersed phase sizes (using Image J Software) are displayed in Fig. 2 and Fig. 3. In all TEM micrographs, the dark part corresponds to the silicon-rich phases and the bright continuous phase corresponds to the epoxy-amine network.

In all cases, a homogeneous distribution in the epoxy matrix was observed. The POSS®^{Ph}-rich dispersed phase has a spherical or ellipsoidal shape in the different systems with a large diameter distribution ranging from 0.1 to 1.5 μ m for the hybrid epoxy networks containing POSS®^{Ph}-triol. Regarding the literature there is no difference on the



Fig. 2. a) TEM micrograph of the hybrid O/I epoxy network containing POSS®^{Ph}-triol, b) Size distribution of POSS®^{Ph}-triol aggregates.



Fig. 3. TEM micrographs of the hybrid O/I epoxy networks containing: a) IL.Cl-g-POSS \mathbb{R}^{Ph} at different magnification (a₁; a₂), b) IL.NTf₂-g-POSS \mathbb{R}^{Ph} at different magnification (b₁; b₂) and their size distribution (a₃, b₃).

TEM image between any closed inert POSS®^{Ph} and open POSS®^{Ph}-triol, generally inert POSS® remains undispersed or non-homogeneous dispersed and even tends to agglomerate in the mixing system due to the poor interfacial adhesion [73,74]. The POSS®^{Ph}-triol can also form hybrids with large aggregates due to the hydroxyl groups of the open cage (POSS®-triol) that are well hidden because of hydrogen bonds between POSS®-triol particles [75,76]. For this reason, several authors try to use some modifiers (metal complex) for better dispersion [75,76]. The epoxy networks containing IL-g-POSS®^{Ph} on the other hand have a narrower diameter distribution ranging only from 10 to 100 nm whatever the chemical nature of the counter anions (Cl⁻ or NTf₂). According to the literature, various authors demonstrated that IL-functionalized silica nanoparticles having different counter anions (Cl⁻ and MeSO₃) led to well dispersed silica aggregates having a size of few tens of nanometers [37,38,77]. Thus, as for nanocomposites based on silica nanoparticles, the imidazolium ILs act as efficient interfacial agents for inorganic-rich nano-objects in epoxy-amine networks.

3.3. Thermomechanical properties of the resulting networks

The influence of the unmodified and modified POSS®^{Ph} on the

thermomechanical properties of the epoxy-amine networks was investigated by Dynamic Mechanical Analysis (DMA) (Fig. 4a). The dynamic mechanical spectra of the different epoxy networks allow to determine the storage and loss moduli, as well as the tan δ relaxation peaks (T_{β} , T_{α}) over a temperature range spanning from -100 to 250 °C. For all the epoxy networks, the narrowness of the main relaxation peak (T_{α}-associated to the glass transition) in the 160–170 °C temperature range suggests that the epoxy-amine networks display a homogeneous structure [19,78]. Moreover, all the epoxy networks exhibit a secondary transition at - 60 °C corresponding to β -relaxation which is attributed to the local motions of hydroxyether [-CH2-CH(OH)-CH2-O-] and bisphenol-A units of the epoxy-amine network [79]. The hybrid O/I epoxy network containing POSS®^{Ph}-triol displays the lowest temperature of the α -transition (160 °C) as well as the lowest shear modulus in the rubbery state, G'_c (Fig. 4b). This observation suggests that POS-S®^{Ph}-triol displays poor interactions at the epoxy-amine network/-POSS®-rich dispersed phase interface, in agreement with the previously observed morphologies. Indeed, the reaction between the hydroxyl groups from POSS®^{Ph}-triol and epoxy functions from the DGEBA prepolymer requires specific conditions to occur, like those reported by Hongzhi et al. [76] who obtained epoxy-POSS®^{Ph}-triol networks only



Fig. 4. a) Dynamic mechanical spectra and b) the shear storage moduli, G'c (at 200 °C) of the epoxy-amine and the hybrid O/I epoxy networks containing $POSS \mathbb{R}^{Ph}$ -triol and IL-g- $POSS \mathbb{R}^{Ph}$ with different anions (Cl⁻ and NTf₂) at 1 Hz.

through the use of a metal complex, aluminum triacetylacetonate (Al), as catalyst. The DMA results are also in a good agreement with the DSC measurements as only one glass transition temperature could be evidenced (see Fig. S5 in the SI). The shear storage moduli, G'c (Fig. 4b), of the rubbery hybrid O/I epoxy networks containing IL-g-POSS®^{Ph} with different anions are slightly higher than the one of the neat epoxy possibly due to a nanoreinforcement effect and a slightly increased crosslinking density. Such behavior is a direct consequence of both chemical bonding and physical interactions generated at the O/I interface, *i.e.* between the ionic liquid-grafted POSS®^{Ph} nano-objects and the epoxy network as well as between POSS® cages and their phenyl ligands [23].

3.4. Mechanical properties

a. Elastic and large strain mechanical properties

The influence of the presence of non-modified and IL-grafted POSS \mathbb{R}^{Ph} on the uniaxial compression response of the different epoxy networks was studied. The values of Young's modulus, yield stress, strain and stress at break are summarized in Table 2. In addition, the stress-strain curves are given in Fig. 5.

The addition of $\text{POSS} \otimes^{\text{Ph}}$ -triol improves all the measured quantities. However, the presence of IL-g- $\text{POSS} \otimes^{\text{Ph}}$ nanoclusters with both anions (Cl⁻ and NTf₂) induces an even better reinforcement effect. Increasing both stiffness, yield strength, and the ability to sustain larger deformation and stress at break is not a common feature for highly crosslinked networks even less when they are filled with inorganic nano-objects [80, 81]. For example, Donato et al. [77] considering epoxy-silica nano-composites and using different imidazolium ILs only as free additive catalysts, reported lower improvements for much higher silica contents (7.5 wt %), *i.e.* an increase in the Young's modulus and strain at break up

Table 2

Mechanical properties of the neat epoxy-amine and the hybrid O/I epoxy networks measured under uniaxial compression (1 mm min⁻¹; 25 $^\circ$ C).

Material	Young's modulus (GPa)	Yield stress (MPa)	Stress at break (MPa)	Strain at break (%)
Epoxy-amine Epoxy-amine/ POSS® ^{Ph} -triol	$\begin{array}{c} 2.3\pm0.1\\ 2.9\pm0.1\end{array}$	$\begin{array}{c} 114\pm9\\ 131\pm9 \end{array}$	$\begin{array}{c} 114\pm 4\\ 141\pm 6\end{array}$	$\begin{array}{c} 28\pm2\\ 31\pm2 \end{array}$
Epoxy-amine/IL. Cl-g-POSS® ^{Ph}	$\textbf{3.0} \pm \textbf{0.1}$	166 ± 11	174 ± 3	40 ± 3
Epoxy-amine/IL. NTf ₂ -g-POSS® ^{Ph}	3.1 ± 0.1	170 ± 10	164 ± 5	40 ± 2



Fig. 5. Stress-strain curves of the neat epoxy-amine and the hybrid O/I epoxy networks.

to 2 and 41%, respectively. The same group also reported significant improvements of mechanical properties (Young's modulus increased 7% and strain at break increased 47%) by grafting imidazolium IL combined with different anions (Cl⁻ and MeSO₃) onto silica particles and with less content of each IL-silica (<6.8 wt %) [38]. We hypothesize the improved properties we obtained are due to the very fine dispersion of the IL-grafted POSS®^{Ph} nanoclusters into the epoxy-amine network as well as to the strong interactions formed at their interface. Indeed, the grafted imidazolium-based ILs reduce the POSS®^{Ph} aggregation and generate a strong and reversible interaction between nanoclusters and the epoxy-amine matrix. The mutual dipole-ion interaction between IL-g-POSS®^{Ph} nanostructures and the network chains enables a higher cohesion and can sustain larger stresses and strains before breaking.

b. Fracture properties

The influence of the non-modified and IL-modified POSS \mathbb{R}^{Ph} on the stress intensity factor, K_{IC} , and fracture toughness, G_{IC} , of epoxy-based networks was investigated using compact-tension fracture test (CT). The values of the critical stress intensity factor, K_{IC} , of neat epoxy-amine and epoxy hybrid O/I networks are summarized in Table 3.

The fracture properties of the neat epoxy-amine network are in agreement with the literature [63,82,83]. In the case of the hybrid O/I epoxy networks based on the different types of $POSS \ ^{Ph}$, two different behaviors are observed. The hybrid network containing the POS- $S \ ^{Ph}$ -triol displays lower fracture properties compared to the neat

Table 3

Fracture properties of the neat epoxy-amine and the hybrid O/I epoxy networks.

Material	K _{IC} (MPa m ^{1/2})	G_{IC} (J m ⁻²)
Epoxy-amine	0.71 ± 0.08	250 ± 40
Epoxy-amine/POSS® ^{Ph} -triol	0.61 ± 0.08	150 ± 40
Epoxy-amine/IL.Cl-g-POSS® ^{Ph}	1.02 ± 0.06	390 ± 30
Epoxy-amine/IL.NTf ₂ -g-POSS® ^{Ph}	$\textbf{0.98} \pm \textbf{0.06}$	350 ± 30

epoxy-amine network whereas the hybrid O/I epoxy networks containing IL-g-POSS $^{\mathbb{R}^{Ph}}$ exhibit higher K_{IC} and G_{IC}. As shown in Fig. 3, this difference can be attributed to the smaller (10-100 nm) and more uniform and well-dispersed $\text{POSS} \ensuremath{\mathbb{R}}^{Ph}$ aggregates for IL-g-POSS $\ensuremath{\mathbb{R}}^{Ph}$ hybrids whatever the nature of the anion (Cl⁻ or NTf₂) as well as to their improved interfacial interactions. While, the non-grafted POSS®^{Ph}, which are assembled in larger (up to micron-size) and less cohesive aggregates, act as local defects leading to a lower crack propagation resistance. According to the literature, ILs can act as dispersing agents for high-T_g thermoplastics [84], core-shell particles [85,86], or nanoparticles added to epoxy networks and have a significant influence on the fracture toughness of the modified networks [77,84,87–89]. Also, as K_{IC} is known to be strongly affected by the nanocomposites morphology and interfacial characteristics, a fine dispersion of such stiffer fillers ensures the promotion of efficient toughening mechanisms: increase of the process zone size, crack pinning and branching leading to a deviation of the crack propagation [38,77,90].

3.5. Surface properties

Surface energies of the neat epoxy-amine and the hybrid O/I epoxy networks were determined by the sessile drop method using Owens-Wendt theory [64]. Therefore, the non-dispersive and dispersive components were calculated from the water and methylene diiodide contact angles (Table 4).

In all cases, the addition of 5 wt % of unmodified (POSS $\ensuremath{\mathbb{R}}^{Ph}\xspace$ -triol) or IL-grafted modified POSS®^{Ph} leads to a decrease of the surface energy, which results from the combined reductions of the dispersive and nondispersive components. These results can be explained by the hydrophobic character of the POSS® molecules composed of phenyl ligands [91]. However, the grafting of POSS®^{Ph} with imidazolium ionic liquids also plays a key role in the hydrophobicity of the epoxy network as shown by the significantly decreased surface energy for systems containing IL-modified POSS®^{Ph} (Table 4). Indeed, the values obtained here are similar to the ones measured for different fluorinated polymers such as PTFE [92]. This surface behavior can be clearly attributed to the presence of the imidazolium IL which is well-known to have low surface tension [93]. According to the literature, the incorporation of various amounts of phosphonium or imidazolium ILs into epoxy networks leads to the formation of highly hydrophobic networks opening many perspectives in the field of paints and coatings. These surface energy are also lower than ones measured on epoxy modified by fillers with 3.5 phr

Table 4

Determination of dispersive and non-dispersive components of the surface energy of the neat epoxy-amine and the hybrid O/I epoxy networks from contact angles with water and methylene diiodide.

Samples	Θ _{Water} (°)	Θ _{CH2I2} (°)	γ non-dispersive (mJ m ⁻²)	γ dispersive (mJ m ⁻²)	γ_{total} (mJ m ⁻²)
Epoxy-amine	79	49	4.8	34.8	39.6
Epoxy-amine/ POSS® ^{Ph} -triol	96	51	0.7	33.4	34.1
Epoxy-amine/IL. Cl-g-POSS® ^{Ph}	99	64	0.4	26.2	26.6
Epoxy-amine/IL. NTf ₂ -g- POSS® ^{Ph}	105	67	0.5	22.7	23.2

of silica [94] or 10 phr of amphiphilic triblock copolymer bearing a poly (butadiene-g-POSS® block) [95]. Similar results were also found in the literature when using high amount (10 wt %) of POSS®-capped poly (ethylene oxide) [96,97].

3.6. Thermal-oxidative stability

The weight loss as a function of temperature under air atmosphere as well as the initial decomposition temperature ($T_{d5\%}$) and the maximal degradation temperature (T_{dmax}) of the hybrid O/I epoxy networks was measured by TGA and are presented in Fig. 6a and b.

The TGA traces of the hybrid O/I epoxy networks display the same decomposition behavior as the neat epoxy-amine network, which is characterized by two decomposition steps. The first and biggest weight loss occurs from 350 to 500 °C corresponds to the simultaneous decomposition of the organic matrix, IL, and phenyl ligands of the POSS® cages as well as the formation of carbonaceous compounds. During the second step of thermal degradation occurring from 500 to 650 °C, these carbonaceous compounds are eventually oxidized and volatilized [98]. An increase of the thermal stability of epoxy networks containing POSS®^{Ph} nano-objects compared to the neat epoxy-amine network is clearly observed. It is worth noting that the epoxy/IL-g-POSS®^{Ph} hybrids with different anions types exhibit a higher stability compared to the epoxy/POSS®^{Ph}-triol hybrid. In addition, the presence of the NTf2-anion improves better the thermal stability, especially the resistance to oxidation during the second step (see Fig. 6b). This phenomena can be explained from the existence of improved interfacial interactions between the epoxy matrix and the IL-grafted $\text{POSS} \ensuremath{\mathbb{R}}^{\text{Ph}}$ [99,100] and the nanoscale dispersion of the later nano-objects acting as a more efficient barrier against heat and oxygen transport [22]. In fact, well-dispersed POSS® nanoclusters at the molecular level can suppress mass loss from segmental decomposition via gaseous fragments. Such behavior is very similar to the one reported in the literature for fully exfoliated clay-polymer nanocomposites [33]. In summary, a real synergistic effect between POSS®^{Ph} and ionic liquids takes place leading to a significant increase of the thermal stability of the resulting networks.

3.7. Fire resistance

- a. **Flammability** data from PCFC tests are listed in Table 5 and HRR curves are plotted versus temperature in Fig. 7 for the different hybrid O/I epoxy networks.
- b. **Fire behavior** of the neat epoxy-amine, the hybrid O/I epoxy networks was evaluated with cone calorimeter experiments, closer to real-word fire conditions. Indeed, PCFC cannot assess some phenomena as barrier effect. The HRR curves, displayed in Fig. 8, come as a support for Table 6 that lists the following data extracted from the cone calorimeter tests: time to ignition (TTI, in second), total heat released (THR, in kJ g⁻¹), peak of heat release rate (pHRR, in kW m⁻²), residual weight (RW in %), effective heat of combustion (EHC, in kJ g⁻¹), and total smoke released (TSR in m⁻²). Inspection of the char residues morphology was also carried out.

Peak of heat release rate (pHRR) and Total heat release (THR) are respectively 559 W g⁻¹ and 29.4 kJ g⁻¹ for the neat epoxy-amine network and are in a good agreement with previously published data [101]. The O/I hybrid epoxy network containing POSS®^{Ph}-triol does not exhibit much better flammability properties. In fact, pHRR is just slightly lower and appears at the same temperature while THR is reduced to 26.9 kJ g⁻¹. Nevertheless, the residue content is slightly increased (from 6 to 15 wt %). Both hybrid O/I epoxy networks containing IL.Cl-g-POSS®^{Ph} and IL.NTf₂-g-POSS®^{Ph} also show better performances than the neat epoxy-amine network and the network containing POSS®^{Ph}-triol. Even if the temperature at peak is similar for both hybrids, epoxy-amine/IL.NTf₂-g-POSS®^{Ph} also appears to be



Fig. 6. a) Weight loss (TGA) and b) derivative of TGA curves (DTG) as a function of temperature for the neat epoxy-amine and the hybrid O/I epoxy networks under air atmosphere ($10 \degree C min^{-1}$).

Table 5			
PCFC data of the neat epoxy	-amine and the h	ybrid O/I epox	v networks.

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Material	pHRR (W g ⁻¹)	TpHRR (°C)	THR (kJ g ⁻¹)	Residue (wt %)	Δh (kJ g ⁻¹)
Epoxy-amine	559	382	29.4	6	31.1
Epoxy-amine/ POSS® ^{Ph} -triol	498	379	26.9	15	31.6
Epoxy-amine/IL. Cl-g-POSS® ^{Ph}	418	447	26.5	9	29.2
Epoxy-amine/IL. NTf ₂ -g-POSS® ^{Ph}	409	449	21.9	14	25.5



Fig. 7. PCFC HRR traces of the neat epoxy-amine, and the hybrid O/I epoxy networks.

slightly more thermally stable at low temperatures (in the range 350–450 °C). Heat of complete combustion, Δh , is in the range 29–32 kJ g⁻¹, except for epoxy-amine/IL.NTf₂-g-POSS®^{Ph} (25.5 kJ g⁻¹) confirming once again its best flammability-resistance. One can notice that no additional peak is evidenced at high temperatures (above 500 °C) as observed in TGA. In fact, the second TGA peak is attributed to the thermo-oxidation of residues while pyrolysis in PCFC is performed under anaerobic conditions thus inhibiting this second step.

TTI is used to determine the influence of a flame-retardant on ignitability. For the hybrid O/I networks, TTI does not decrease in comparison to neat epoxy-amine network. Such a stability of TTI is very valuable for enhancement of the flame-retardancy properties of epoxy resins [30]. Indeed, phosphorus compounds are efficient fire-retardant additives promoting charring and reducing heat release rate in epoxy resins; unfortunately, most of them also enable an earlier ignition due to



Fig. 8. Cone calorimeter HRR curves of the neat epoxy-amine, and the hybrid O/I epoxy networks.

Table 6

Cone calorimeter	data	of the neat	epoxy-amine,	the hybrid	O/I epoxy	networks.
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Material	TTI (s)	THR (kJ g ⁻¹)	pHRR (kW m ⁻²)	RW (%)	EHC (kJ g ⁻¹)	TSR (m²)
Epoxy-amine	82	22.2	1084	11.5	25.1	25.0
Epoxy-amine/ POSS® ^{Ph} -triol	92	22.2	983	11.7	25.1	25.1
Epoxy-amine/IL. Cl-g-POSS® ^{Ph}	94	20.7	480	6.3	22.2	24.1
Epoxy-amine/IL. NTf ₂ -g- POSS® ^{Ph}	106	20.8	508	9.8	23.2	23.1

the deterioration of epoxy thermal stability by phosphoric acids while the present materials avoid this drawback.

HRR curves for a, and b (Fig. 8) show a sharp pHRR followed by a fast decrease to flame out. Such curves are indicative of a fast and uncontrolled burning. The neat epoxy-amine network is highly flammable and the HRR shows a sharp peak heat release rate (pHRR) of 1084 kW m⁻². When the POSS®^{Ph}-triol is added, the pHRR remains close to 1000 kW m⁻² while the two IL-g-POSS®^{Ph} modified epoxy networks exhibit a significant decrease. In several cases, a second peak is observed at the end of the test. pHRR for c and d are much lower (480 and 508 kW m⁻²) and a progressive decrease of HRR is observed from 250 s to flame out due to slow thermo-oxidation of the residue (flame is reduced and does not cover the whole sample, therefore thermo-oxidation can occur). These curves show that these samples highlight a so-called thick-

charring behavior, *i.e.* the accumulation of a stable residue limiting the heat transfer from the flame to the outer part of the material slowing down its pyrolysis [101]. The lack of additional peak at the end of burning may be ascribed to a quite good protective effect of the residue.

The combustion efficiency, *i.e.* the ratio between the effective heat of combustion and the heat of complete combustion measured in PCFC, is in the range of 0.76–0.90 for polymeric materials. It is not significantly lower for epoxy-amine containing IL.Cl-g-POSS®^{Ph} despite the release of chlorine-containing gases. Chlorine is not detected in the residue from EDX analyses. Nevertheless, this halogen is well known to act as flame poisoner but is probably in too low content to be effective here.

Photographs of post-fire residues obtained after the cone calorimeter experiments are shown in Fig. S6 in the SI. As can be seen, the neat epoxy-amine, and the hybrid O/I epoxy containing POSS®^{Ph}-triol and IL.Cl-g-POSS®^{Ph} networks left a small and poorly cohesive dome-like char whose top part has collapsed. On the contrary, for the hybrid O/I epoxy containing IL-g-POSS®^{Ph} with NTf₂ anion (Fig.S6d of SI, the residue has swollen distinctly, and the top layer is white and still seems protective. EDX and SEM analysis were carried out on the upper and lower layers of the residue for the epoxy-amine/IL.NTf_2-g-POSS $\ensuremath{\mathbb{R}}^{Ph}$ network (Fig. S7 of SI). On one hand, the top layer appears as a dense porous homogeneous network. More surprisingly, it does not contain carbon and the proportions of oxygen and silicon are very close to the theoretical ones for silica. We can thus assume this upper surface is pure silica. Such layer is not observed for the other hybrids for which the silicon content in residue remains close to 10 wt %. On the other hand, the bottom surface of epoxy-amine/IL.NTf₂-g-POSS®^{Ph} is completely different and exhibits a composition closer to the original network. Such a top layer may be mechanically stable enough to enhance the fire resistance of the composite material, but this assumption needs further investigation.

The whole burning process was recorded using both an optical and a thermal camera to get new insights on the decomposition kinetics of the epoxy containing IL-g-POSS $\ensuremath{\mathbb{R}}^{Ph}$ (note that the pictures and the temperature curves do not correspond exactly to the HRR curves in Fig. 7 because the distance between radiant cone and samples was increased from 25 to 60 mm). The optical pictures in Fig. S8 of SI follow the combustion of the hybrid O/I epoxy networks containing IL.NTf2-g- $POSS \ensuremath{\mathbb{R}}^{Ph}$ and $IL.Cl-g-POSS \ensuremath{\mathbb{R}}^{Ph}$ respectively. It can be seen that the expansion of both char layers occurs slowly and only around 200 s, i.e. well after the peak of heat release rate, when the HRR is decreased at a lower level. It means that the expansion is not responsible for the better fire performances of these materials. For epoxy-amine/IL.NTf2-g-POSS®^{Ph}, the flames are observed shortly after and only on the edges of the sample. Therefore, thermo-oxidation can occur and char is progressively removed from the surface, which becomes white (i.e. corresponding to the silica layer, as discussed above). Nevertheless, the surface remains cohesive without any cracks. In contrast, for epoxyamine/IL.Cl-g-POSS®^{Ph}, cracks are observed very quickly (after 200 s white arrow) but the cracks develop slowly and the char residue fully breaks only at the end of the test.

Fig. 9 shows the pictures of both networks recorded from the thermal camera. While the surface appears unchanged during the whole test for epoxy-amine/IL.NTf₂-g-POSS®^{Ph}, the formation of cracks (indicated by a white arrow) and the final breaking of the residue layer is clearly shown for epoxy-amine/IL.Cl-g-POSS®^{Ph} confirming the observations from Fig. S8-b in the SI.

As a conclusion, the use of ionic liquid grafted onto the POSS®^{Ph} cages whatever the nature of the anion (Cl⁻ or NT⁶₂) gives a significant enhancement on the pHRR compared to the neat epoxy network. These results are much better than those of epoxy-amine/POSS®^{Ph}-triol modified with the aluminum triacetylacetonate (Al) [5,98] or with 9, 10-dihydro-9-oxa-10-phosphaphenanthrene-10-oxide (DOPO) [30, 102]. A similar effect was also found in fully layered silicate-epoxy nanocomposites but with higher ignitability [103,104]. This enhancement on fire behavior can be explained not only by the nanodispersion of



Fig. 9. Pictures obtained using thermal camera from cone calorimeter test of the hybrid O/I epoxy networks containing $IL.NTf_2$ -g-POSS®^{Ph} and $IL.Cl-g-POSS®^{Ph}$.

 $POSS \ensuremath{\mathbb{R}}^{Ph}$ moieties but also by the nature of the IL (cation/anion) associated to the $POSS \ensuremath{\mathbb{R}}^{Ph}$ cages, which affects the thermal stability and the combustion process [30]. Even if pHRR is in the same range for both epoxy networks containing IL.Cl-g-POSS $\ensuremath{\mathbb{R}}^{Ph}$ and IL.NTf₂-g-POSS $\ensuremath{\mathbb{R}}^{Ph}$, it can be assumed that IL-g-POSS $\ensuremath{\mathbb{R}}^{Ph}$ with NTf₂ anion allows creating a well-organized and compact residue on the top surface of the epoxy composite, which may limit more efficiently the heat diffusion in the condensed phase in other fire conditions.

4. Conclusions

In this work, IL-grafted polyhedral oligomeric silsesquioxanes (IL-g-POSS®^{Ph}) were successfully designed and used as modifiers of a standard epoxy-amine network (DGEBA/IPD). The incorporation of a low amount (5 wt %) of such organic-inorganic and ionic hybrid nanoobjects lead to the fine nanostructuration of multifunctional epoxybased thermosets. We demonstrated that the chemical nature of the counter anion, i.e. chloride (Cl⁻) versus bistriflimide (NTf₂), has no influence on the polymerization kinetics. However, due to the catalytic effect of the IL, it plays a key role on the final properties of the resulting networks thanks to the formation of strong interactions between the epoxy network and the IL-grafted POSS®^{Ph}. The introduction of IL-g-POSS®^{Ph} thus contributed to a significant improvement of the mechanical properties of the obtained networks, i.e. both stiffness and toughness were increased without any decrease of the glass transition temperature. Moreover, the fire retardancy of the hybrid O/I epoxy networks was also more specifically evaluated from pyrolysiscombustion flow calorimetry (PCFC) and cone calorimeter analyses. These first results clearly highlighted the promising synergistic effect of POSS®^{Ph} nanoclusters combined to imidazolium ILs inducing impressive reductions of the pHRR (55%) and an important retardancy effect by significantly increasing the ignition time. Hence, IL modified POSS® can be envisioned as a novel alternative for FR additive that non-only shows efficient fire resistance capabilities but also improves the mechanical properties of the obtained epoxy composite. Finally, the grafting of POSS®^{Ph} by ILs definitely opens new interesting perspectives in the fine-tuning of interfacial interactions of polymer nanocomposites.

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Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Appendix A. Supplementary data

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