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Fire behaviour of electrical cables in cone calorimeter: Influence of cables structure and layout

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ABSTRACT

The fire performances of small telecom halogen-free cables were measured using cone calorimeter by changing several test conditions (heat flux, number and spacing of cables) and cable properties (sheath thickness and insulation mass). An analytical phenomenological fitting was proposed to predict accurately main fire performances (time-to-ignition, peaks of heat release rate and time to peak of heat release rate) from a set of 42 tests. The phenomenological model also assesses quantitatively the influence of different test conditions and cable properties. It appears that time-to-ignition is only dependent on heat flux. Moreover the influence of sheath is pointed out to delay the occurrence of the main peak of heat release rate corresponding to the decomposition of non-flame retarded insulation. The fitting allows better predicting the fire hazard in case of cables burning.

Keywords:

Wire and cable flammability
Fire performances prediction
Cone calorimeter
Cable design

1. Introduction

In the fire statistics, electrical appliances are one of the main sources of fire. In such fires, the first ignited component is the insulation around wires and cables. From 2003 to 2005, 46% of US electrical fires are caused by electronic wiring, and 350 lives each year are lost because of old unsuitable wires [1]. The same conclusions can be made for the European Union, and in order to protect installations and people, new regulations concerning fire safety were developed. In European Union, cables used in buildings are covered by the Construction Product Regulation since 2013. To be ready for the CE marking cables have to pass reaction to fire tests as the large-scale flame test EN50399. Those large-scale tests are time-consuming and so, very expensive. Therefore, one alternative is to determine first the fire behaviour of these cables with laboratory-scale fire tests. If those tests are promising, large-scale fire tests are run to properly classify the cables.

Before being rated through large-scale tests, cables and more especially sheath materials are often assessed using small-scale lab tests such as Limiting Oxygen Index (LOI) [2], cone calorimeter [3–11], thermal analysis [9,12,13] and more recently microscale calorimeter (MCC) [14–18]. Other less conventional small and intermediate scale tests or methods have been also developed and used [19–24]. With regard to LOI, a common statement reports that cable sheathing exhibiting LOI value over 30 enables cables to meet most of large scale tests [2]. However the authors highlighted that correlation between

small and large scale tests is poor because cable tests depend on other parameters than the sheath properties (i.e. inner layer, cable layout ...).

MCC was developed to assess the flammability of polymers using only few milligrams of material. This technique has been already used to study the burning properties of materials composing cable sheath [16–18]. Correlations between MCC data and conventional flammability tests for wire and cable compounds have been investigated [14,15]. Cogen et al. studied correlation between MCC and flame spread tests performed on seven halogen-free FR compounds used for cable sheathing. Temperature at pHRR measured by some PCFC data can supply rough indication for flame spread test ranking. However correlation between absolute values remains poor because cable structure cannot be taken into account [15].

Cone calorimeter is a bench-scale equipment that was demonstrated to be relevant to estimate the full-scale fire behaviour of various products including cables [3,4,25]. Hirschler [26] and afterwards Barnes [6,7] investigated the behaviour of a series of 21 electric cables exhibiting the same layout but differing only by the composition of their sheath or insulation using the cone calorimeter test (ISO 5660) and the large-scale tests (ASTM D5424, FT4 protocol). A good correlation was observed between the two tests regarding peaks of HRR data for cables passing the large-scale test. On the contrary, a wide dispersion was noted for cables that failed the large-scale test. Coaker et al. [5] found a good correlation between full scale cable tray tests and cone calorimeter, both in terms of heat and smoke release, in the case of various

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Abbreviations

A, B, C, D, E	names of cables (from cables of house telecom network)
S	sheath thickness (mm)
I	insulation mass presents in one cable (g)
N	number of cables in the sample holder
d	density of cables
HF	heat flux of cone calorimeter tests (kW/m^2)
HRR	heat release rate (kW/m^2)
EHC	Effective heat of combustion (MJ/kg)
MLR	Mass Loss Rate (g/s)
TTI	time of ignition (s)

Δt	time difference between time of ignition and time of pHRR1 (s)
pHRR ₀	first peak of heat release rate (kW)
pHRR ₁	second and biggest peak of heat release rate (kW)
X _α Y _{HFβ}	the cable X is tested. α Number of cables are used in the test
Y	is the configuration of cables in sample holder
T	configuration of cables that are assembled together without any space between them
Sω	configuration of cables when ω spaces separate each cable. The heat flux of the cone is equal to β kW/m^2
Z*	quotient for parameter Z of a test divided by the parameter Z for the reference test A ₆ sp1D_HF50

cables containing vinyl compounds. The correlation was particularly good using low external heat flux, i.e. 20 kW/m^2 . Afterwards further studies confirmed that cone calorimeter was a powerful test to investigate the fire behaviour of cables [8,27,28]. Hence works were carried out to develop test procedures aiming at supplying good practice when using this instrument for cables [29,30].

The cable structure and layout are important parameters that may influence the development of a fire and thus the fire hazard. Cone calorimeter is likely to enable testing such parameters. However, only few papers can be found in the literature on this topic. Concerning cable layout, Elliott and Whiteley studied small diameter wires with different tests design inside the sample holder of the cone calorimeter [31]. Cables were randomly or symmetrically wrapped and arranged in one or several layers. Two configurations seemed to be repeatable enough, economical both in terms of amount of sample and time for preparation, permitting data analysis: a single layer of parallel touching cables, and a configuration with repetitive touching units of seven twisted cables. This last design was possible because of the flexibility of the studied cable. Other research groups studied power cables, communication cables, data cables and wires thicker than the previous work of Elliott and Whiteley. They mainly studied the combustion of these electric cables with a position side by side, the number of tested cables was driven by the outer diameter of the cable [3,8,27]. Meinier et al. studied the role of spacing in the fire behaviour of large halogen-free cables in cone calorimeter [11]. They found that spacing has a significant (but not linear) influence on the whole HRR curve.

With regard to cable structure, Rao et al. studied the fire behaviour of cables exhibiting various outer sheaths and constructions (number of outer layers, layer thickness) [32]. All these parameters were shown to have an effect on the cone data and HRR curve. The same research group evidenced that the sheath thickness influences the burning time and the smoke production that were shown to vary almost linearly with thickness [33]. As explained above, not only the sheath material but also the other components and the cable structure itself have a significant influence on the fire behaviour [9,30]. Meinier et al. [11] showed that the fire hazard increases significantly when the inner part (generally non flame retarded polyethylene) starts pyrolyzing. Hence the role of the inner components should not be neglected. Gallo et al. [34] used a new test based on the cone calorimeter equipment where the cone heater was replaced by a burner and a portion of cable tray in vertical position was tested. They evidenced that the HRR curve of the entire cable can be predicted from the curve of its different components.

Finally test conditions, and especially heat flux, have an important effect on cable flammability. Generally, ignition occurs earlier and heat release rate is higher when heat flux increases [10,28,33]. Nevertheless, a more specific effect was found by Meinier et al. [11]. Indeed, a heat flux threshold is needed to promote the burning of the inner insulation part of cables. Below this threshold, only the sheath is decomposing and the heat release is limited. But above this threshold, non-flame retarded insulation burns leading to much higher heat release.

In this paper, the role of cable structure and cable layout on the fire behaviour of a series of relatively thin halogen-free cables was thoroughly investigated. The burning behaviour of cables was studied using cone calorimeter and described thanks to four representative properties. An analytical fitting was proposed to predict the main flammability properties of cables taking into account the respective influence of each parameter investigated.

2. Materials and methods

2.1. Cables

The samples used in this study were telecom cable-types provided by ACOME, cable, wire and synthetic tubes manufacturing French company. Fig. 1 and Fig. 2 describe the global structure of the studied wires, in which different parameters can differ (the sheath thickness and the insulation mass). Table 1 lists the different cables used in this publication. These cables are halogen-free ones. The sheath material is based on EVA and PE matrix filled with high amount of aluminium trihydroxide (ATH). The insulation is pure polyethylene. It does not contain any flame retardant species. More details about the exact composition are confidential.

2.2. Cone calorimeter

The study of cable fire performances was inspired by the ISO 5660-1 standard with Cone Calorimeter provided by Fire Testing Technology Limited [35]. Different heat fluxes were used: 25, 50, 80 kW/m^2 . Some additional tests at heat fluxes of 35 and 65 kW/m^2 were also used. Tests were carried out in air under well ventilated conditions (air flow rate 24 L/s), with a piloted ignition and were repeated at least three times.

An adapted setting was used for the cables in the sample holder as shown in Fig. 3. The samples were positioned horizontally, attached to a grid with a mesh size of $2 \text{ cm} \times 2 \text{ cm}$ and a wire diameter of 2 mm .

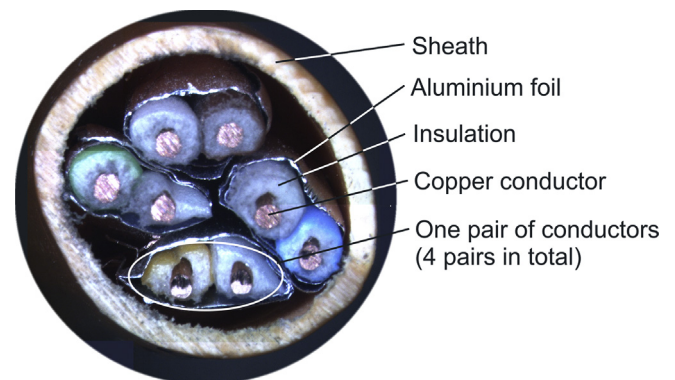


Fig. 1. Cross-section of reference cable (cable A).

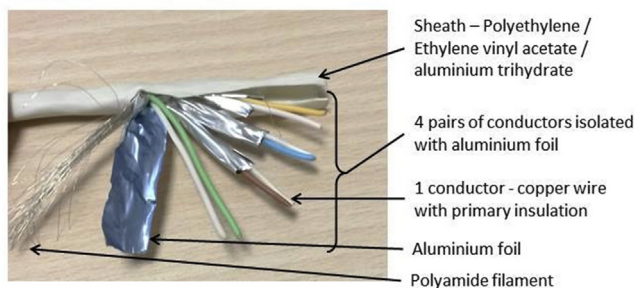


Fig. 2. Description of the reference cable (cable A).

Table 1
Main characteristics of studied cables.

Cables		A	B	C	D	E
Material characteristics	Cable diameter (mm)	7.4	7	7.7	7	7
	Sheath thickness S (mm)	0.55	0.48	0.7	0.5	0.5
	Insulation mass per cable I (g/m of cable)	7	7	7	5.8	5.5
	Copper mass per cable (g/m of cable)	19.4	19.4	19.4	21.6	19.3
Mass fraction of the components of the cables (%)	Sheath	38	34	44	34	36
	Insulation	15	15	13	12	13
	Copper	40	43	36	47	43
	Aluminium foil and polyamide filament	7	8	7	7	8



Fig. 3. Samples of cables attached to a grid – aluminium folder is placed between the grid and the sample holder.

The cables were disposed in the sample holder in different ways. Different amounts of cables were tested with different spacing separating each cable. [Tables 2 and 3](#) show the different layouts tested with the cone calorimeter device.

Each test is called according to the following label: $X_{\alpha} Y_{HF} \beta$ where X is the tested cable, α the number of cables, Y is the configuration of cables in sample holder, β the heat flux. T corresponds to a

tight layout (no spacing between cables). ω corresponds to a loose configuration where spacing between cables is ω times the cable diameter. As an example, Fig. 4 shows the HRR curve of the reference test of this publication, A_6S1_HF50. In this test the cable A is used in a configuration 6S1 with 6 cables separated from each other by one cable diameter. The configuration 6S1 allows to test the maximum number of cables (6) with the spacing between cables defined by the European EN50399 standard, which is one of the most important standard for fire tests on cables. The heat flux 50 kW/m^2 is widely used at the cone calorimeter as the reference heat flux to study materials, within the range of external irradiance given in the ISO 5660-1 standard.

The fire performances that were extracted from the curve and considered for analysis are the following:

- Time of ignition named TTI in second
- First peak of heat release rate named pHRR0 in kW
- Highest peak of heat release rate named pHRR1 in kW
- Time between the time to ignition and the time at pHRR1 (Δt) in second

For convenience of further analysis, it was chosen to consider the raw heat release rate expressed in kW. This type of HRR curve was also observed during the European FIPEC project [29]. According to Rao









Table 2
List of the cone calorimeter tests inputs.

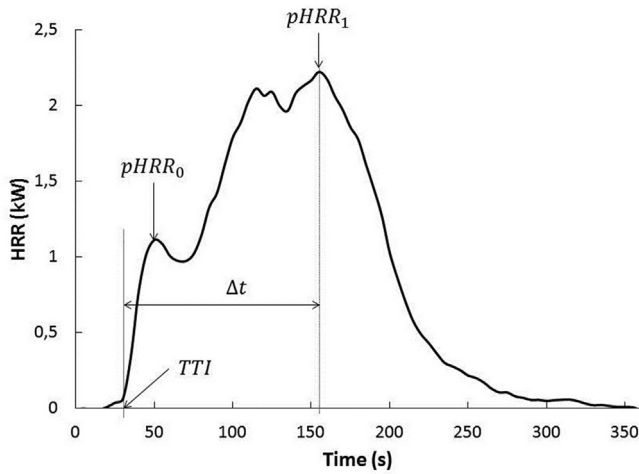
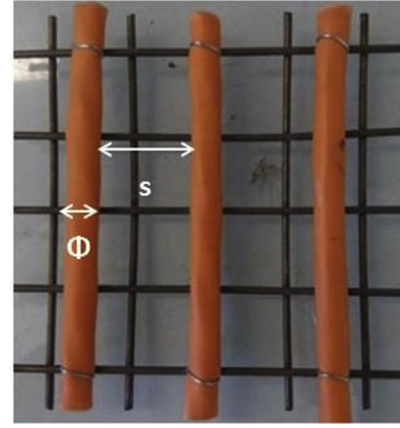
Cable	Configuration	Number of cables (N)	Density of cables (d)	Sheath thickness (S) (mm)	Mass of insulation (I) (g/m of cable)	HF (kW/m ²)
A	6S1	6	0.5	0.55	7	25 35 50 65 80
B				0.48		25 35 50 65 80
C				0.7		25 35 50 65 80
D				0.5	5.8	25 50 80
E					5.5	25 50 80
A	3T	3	1	0.55	7	25 50 80
	6T	6				25 50 80
	12T	12				25 50 80
	3S1	3	0.5			25 50 80
	3S2		0.33			25 50 80
	3S3		0.25			25 50 80
	3S4		0.2			25 50 80

Table 3

Configurations of experiment.

*spacing ω means that two cables are separated by a spacing of ω cable diameters.

Name of the configuration	Number of cables tested (N)	Spacing between each cable*	Picture
12T	12	0	
6T	6	0	
3T	3	0	
6S1	6	1	
3S1	3	1	
3S2	3	2	
3S3	3	3	
3S4	3	4	

**Fig. 4.** Heat release rate of the reference test, where the cable A was tested in a configuration of 6 cables with a spacing equal to one cable diameter between each cable at 50 kW/m², test noted A _ 6 S1 _ HF50.**Fig. 5.** Definition of the parameter density d .

et al., cables show multiple peaks of HRR attributed to the sequenced combustion of the different materials used in the construction of cable. This delay occurs due to a masking effect of the aluminium layer [33]. Braun et al. explained that cables burn in stages (implying multiple pHRR) in function of the layer of the cable assembly actually burning [3]. This hypothesis will be argued in the result section.

2.3. Phenomenological fitting

For fitting purposes, the cone calorimeter results (TTI, pHRR₀, pHRR₁ and Δt) were compiled in this publication as noted in equation (1):

$$Y_{exp} = [TTI, pHRR_0, pHRR_1, \Delta t] = [Y_{exp 1}, Y_{exp 2}, Y_{exp 3}, Y_{exp 4}] \quad (1)$$

Since five experimental and material parameters were varied during the experiments, they are used as variables to describe the fire performances. Parameters can be divided in three categories: (i) test condition parameters namely the heat flux HF , (ii) layout parameters namely the number of cables tested N and the density of cables d , (i.e. the percentage of cable in the repetitive layout, as explained in Fig. 5), (iii) material parameters, or cable properties namely the sheath thickness S and the insulation mass for one cable I .

In order to equally estimate the influence of each parameter, normalised parameters are developed following equation (2). For each test α , they represent the parameter value of the test α divided by the corresponding parameter value from the reference test A _ 6S1 _ HF50:

$$Z_{test \alpha}^* = \frac{Z_{test \alpha}}{Z_{A6S1HF50}} \quad (2)$$

Each parameter HF , N , d , S and I can influence the fire performance, but not necessarily with the same intensity. To take this observation into account, a given fire performance Y_{num} was assumed to be dependent of each parameter according to a power law. The coefficients α , β , γ , δ , ϵ , are the exponents respectively assigned to HF , N , d , S and I . From a numerical point of view, the coefficients quantify the influence of each parameter. Since the resultant function $HF^{*\alpha} \cdot N^{*\beta} \cdot d^{*\gamma} \cdot S^{*\delta} \cdot I^{*\epsilon}$ is dimensionless with values between 0 and 3 (experimental observation), the number 'a' corresponds to the value of Y_{num} obtained for the reference test and is close to Y_{exp} .

$$Y_{num}(a, \alpha, \beta, \gamma, \delta, \epsilon) = a HF^{*\alpha} \cdot N^{*\beta} \cdot d^{*\gamma} \cdot S^{*\delta} \cdot I^{*\epsilon} (a, \alpha, \beta, \gamma, \delta, \epsilon) \epsilon R^6 \quad (3)$$

In order to identify the fittest value of the coefficients, the gap between experimental (eq. (1)) and numerical results (deduced from eq. (3)) was computed via a cost function (denoted J in equation (4)) written as the squared 2-norm for each property to be predicted (i.e. TTI, pHRR₀, pHRR₁ and Δt):

$$J(a, \alpha, \beta, \gamma, \delta, \varepsilon) = (Y_{\text{exp } i} - Y_{\text{num}}(a, \alpha, \beta, \gamma, \delta, \varepsilon))^2, \quad i = 1, 2, 3, 4 \quad (4)$$

Thus the minimization problem given by

$$\min_{(a, \alpha, \beta, \gamma, \delta, \varepsilon) \in \Phi} J_i(a, \alpha, \beta, \gamma, \delta, \varepsilon), \quad i = 1, 2, 3, 4, \quad \Phi = \left[0, +\infty \right] \times [-3, 3]^5 \quad (5)$$

was solved.

Equation (5) was solved using Matlab® software with a constrained Levenberg Marquardt algorithm, which is rather classical in the literature for solving identification problem. It is an algorithm destined to estimate least-squares of non-linear parameters [36]. Unless this problem is highly nonlinear, solutions were reached after 10 iterations with a satisfactory coefficient of determination R^2 as developed in the results and discussion section, independently of the initial parameters values.

As for the experiments, all the cone calorimeter tests inputs are listed in Table 2.

3. Results and discussion

Tables 4 and 5 present the main cone calorimeter results for all the tests carried out. The reported values are the average of at least 3 tests. The phenomenological model described in part 1.3 was successfully applied to this set of experimental data. The best fitted values of the coefficients are given in Table 6. In fact, good fits were found between experimental and calculated values, as evidenced by satisfying R^2 values.

In the following, we will discuss separately each main output of the phenomenological model, namely TTI, pHRR0, pHRR1 and Δt . For information, it can be considered that a parameter Z has a negligible effect on a fire performance Y if the variation of Y_{num} within the studied range of Z^* is lower than 15% which is the higher experimental standard deviation observed (see Tables 4 and 5). Taking into account that Z^* varies at most between 0.4 and 2 (see Table 5), the variation of Y_{num}

is lower than 15% if the exponent of the power law is lower than 0.2.

3.1. Influence of test parameters on TTI

According to the fitting, the time to ignition can be predicted using equation (6). Fig. 6 shows the good agreement between the experimental and predicted TTI values.

$$TTI = 42.25 [HF^{*-2} \cdot N^{*0.1} \cdot d^{*0.01} \cdot S^{*-0.3}] \quad (6)$$

Equation (6) points out that the main influent exponent is the one associated to HF. The absolute values of coefficients associated to other parameters are much lower.

So it appears that only the heat flux significantly influences the time to ignition. Moreover, the TTI linearly depends on HF^{-2} . In literature, the time of ignition was described and predicted with material fire properties and the experimental settings for thermally thick sheets (equation (7)) [37].

$$TTI = \frac{\pi}{4} (k \cdot \rho \cdot c_p) \frac{(T_{ig} - T_0)^2}{HF^2} \quad (7)$$

with k the thermal conductivity of the material, ρ the density, c_p the specific heat, T_{ig} the ignition temperature, T_0 the ambient temperature. The heat flux has to be high enough to ignite the cable.

In conclusion, the simulation gives the same power law as in the physical model. It means that the cables are thermally thick [37–39]. Since their diameter is close to 7 mm, this result appears reasonable. Braun et al. made the same conclusion cables twice as big as our cables [3].

Other parameters have no or negligible influence on time-to-ignition. It means that a small change in cable structure (sheath thickness or PE insulation weight) cannot delay significantly the ignition. Important changes in sheath material or cable structure are needed for this purpose. Moreover a cable tray should ignite similarly under heat flux regardless of its exact configuration (loose or tight layout of the cables, number of cables). Note that in a previous work concerning large halogen-free cables, it was found that spacing had a moderate influence

Table 4
Characteristics of the tests and cone calorimeter results for the cable structure study.

Cable	Configuration	Parameters					Cone Results - Average value				Cone Results - Standard deviation			
		Number of cable (N*)	Density (d*)	Sheath thickness (S*)	Insulation mass (I*)	Heat Flux (HF*)	TTI (s)	pHRR0 (kW)	pHRR1 (kW)	Δt (s)	TTI (s)	pHRR0 (kW)	pHRR1 (kW)	Δt (s)
A	6S1	1	1	1	1	0,5	163	0,82	1,35	127	6	0,07	0,06	7
		1	1	1	1	0,7	75	0,97	1,59	108	0	0,03	0,15	18
		1	1	1	1	1	35	1,12	2,03	81	2	0,01	0,11	2
		1	1	1	1	1,3	28	1,33	2,60	75	1	0,05	0,24	5
		1	1	1	1	1,6	17	1,53	3,10	65	4	0,06	0,20	0,7
B		1	1	0,87	1	0,5	170	0,66	1,47	88	8	0,06	0,14	4
		1	1	0,87	1	0,7	72	0,81	1,76	93	11	0,02	0,04	6
		1	1	0,87	1	1	35	0,97	2,52	81	2	0,006	0,04	12
		1	1	0,87	1	1,3	26	1,16	3,07	72	3	0,07	0,16	15
		1	1	0,87	1	1,6	17	1,28	4,17	63	2	0,03	0,70	3
C		1	1	1,27	1	0,5	148	0,81	1,15	185	6	0,006	0,04	3
		1	1	1,27	1	0,7	71	0,93	1,28	174	1	0,02	0,00	6
		1	1	1,27	1	1	38	1,27	1,68	88	0,6	0,05	0,12	7
		1	1	1,27	1	1,3	31	1,46	2,00	77	2	0,00	0,01	1
		1	1	1,27	1	1,6	17	1,75	2,63	72	2	0,07	0,10	9
D		1	1	0,91	0,83	0,5	175	0,75	1,13	115	3	0,04	0,20	2
		1	1	0,91	0,83	1	47	1,15	1,71	92	5	0,02	0,04	12
		1	1	0,91	0,83	1,6	21	1,49	2,71	59	3	0,11	0,01	3
E		1	1	0,91	0,79	0,5	177	0,80	1,24	120	17	0,03	0,05	16
		1	1	0,91	0,79	1	51	1,10	1,81	89	6	0,08	0,01	23
		1	1	0,91	0,79	1,6	18	1,45	3,40	64	1	0,05	0,55	5

Table 5

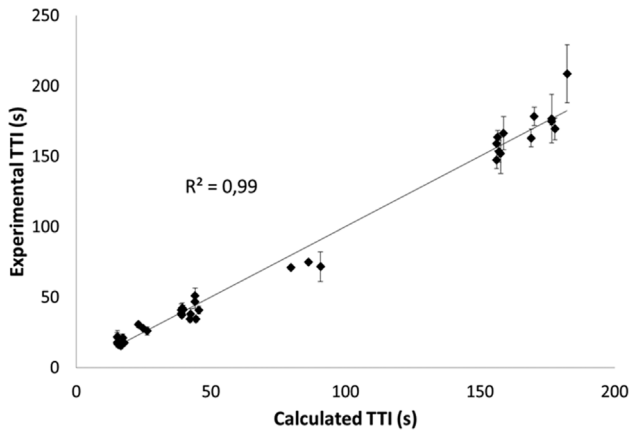
Characteristics of the tests and cone calorimeter results for the study of cone configurations.

Cable	Configuration	Parameters					Cone Results - Average value				Cone Results - Standard deviation				
		Number of câble (N*)	Density (d*)	Sheath thickness (S*)	Insulation mass (I*)	Heat Flux (HF*)	TTI (s)	pHRR0 (kW)	pHRR1 (kW)	Δt (s)	TTI (s)	pHRR0 (kW)	pHRR1 (kW)	Δt (s)	
A	3T	0,5	2	1	1	0,5	166	0,45	1,03	150	12	0,07	0,16	0,7	
		0,5	2	1	1	1	41	0,51	1,84	119	3	0,08	0,16	2	
		0,5	2	1	1	1,6	17	0,73	2,38	79	2	0,03	0,01	5	
	6T	1	2	1	1	0,5	178	0,53	1,50	267	6	0,02	0,15	1	
		1	2	1	1	1	38	0,82	1,99	174	4	0,07	0,10	7	
		1	2	1	1	1,6	16	1,12	2,25	120	2	0,07	0,12	5	
	12T	2	2	1	1	0,5	209	0,58	1,38	304	21	0,03	0,07	17	
		2	2	1	1	1	41	0,97	2,55	192	3	0,07	0,31	5	
		2	2	1	1	1,6	18	1,49	2,99	153	0,7	0,10	0,07	6	
	3S1	0,5	1	1	1	0,5	152	0,67	0,98	93	14	0,07	0,07	9	
		0,5	1	1	1	1	42	0,83	1,82	74	4	0,05	0,21	0,6	
		0,5	1	1	1	1,6	18	1,04	2,93	57	1	0,02	0,10	1	
	3S2	0,5	0,67	1	1	0,5	154	0,64	1,25	67	8	0,03	0,06	8	
		0,5	0,67	1	1	1	38	1,03	2,34	63	2	0,07	0,09	2	
		0,5	0,67	1	1	1,6	22	1,23	3,67	49	2	0,06	0,01	2	
	3S3	0,5	0,5	1	1	0,5	164	0,82	1,53	59	5	0,06	0,07	1	
		0,5	0,5	1	1	1	41	1,09	2,77	59	0	0,14	0,04	0	
		0,5	0,5	1	1	1,6	22	1,28	4,01	41	4	0,11	0,21	0,7	
	3S4	0,5	0,4	1	1	0,5	159	0,51	0,97	51	0	0,11	0,12	7	
		0,5	0,4	1	1	1	41	0,85	1,91	49	4	0,14	0,06	4	
		0,5	0,4	1	1	1,6	22	1,18	2,92	43	3	0,08	0,29	3	

Table 6

Values of the fitting coefficients.

Cone results	α (HF)	β (N)	γ (d)	δ (S)	ε (I)	a	R ²
TTI	-2	0.1	0.01	-0.3	0	42.25	0.99
pHRR ₀	0.59	0.42	-0.31	0.68	-0.57	1.07	0.91
pHRR ₁	0.81	0.14	-0.20	-1	0.94	2.19	0.88
Δt	-0.59	0.39	0.8	1.06	-0.21	89.16	0.94

**Fig. 6.** Experimental versus calculated TTI.

on TTI but only above a threshold spacing value close to one cable diameter (around 12 mm) [11].

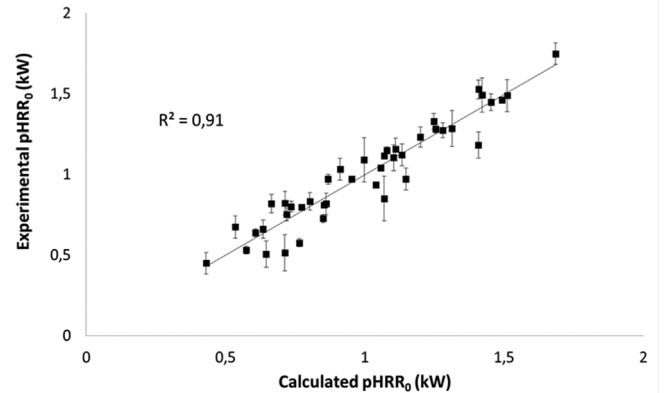
3.2. Influence of test parameters on pHRR₀

Fig. 7 shows the correlation between experimental and predicted pHRR₀ calculated according to equation (8).

$$pHRR_0 = 1,07 [HF^{0,59} \cdot N^{0,42} \cdot d^{*-0,31} \cdot S^{0,68} \cdot I^{*-0,57}] \quad (8)$$

Each parameter has an influence on this first peak of heat release (all the powers are higher than 0.2).

According to Fig. 8, pHRR₀ increases with the sheath thickness (as well as heat flux). As observed by Elliott and Whiteley, a thicker wall means a combustible and the related heat release increase [31]. On the contrary, polyethylene (PE) insulation mass has a reverse influence ($\epsilon = -0.57$). Indeed, a high PE mass insulation decreases pHRR₀. Note that PE is not yet pyrolyzed when pHRR₀ occurs. Fig. 9 shows the effective heat of combustion (EHC) for the reference test A_6S1_HF50. EHC is initially close to 21 kJ/g. This value is close to the EHC of the sheath (23 kJ/g). EHC continuously increases up to around 40 kJ/g (i.e. EHC of pure PE), partly due to the depletion of water released from ATH and partly because the pyrolysis front moves from sheath to insulation. When pHRR₀ occurs at 50s, EHC is still close to EHC of sheath, evidencing that insulation did not start to degrade. Other studies

**Fig. 7.** Experimental versus calculated pHRR₀.

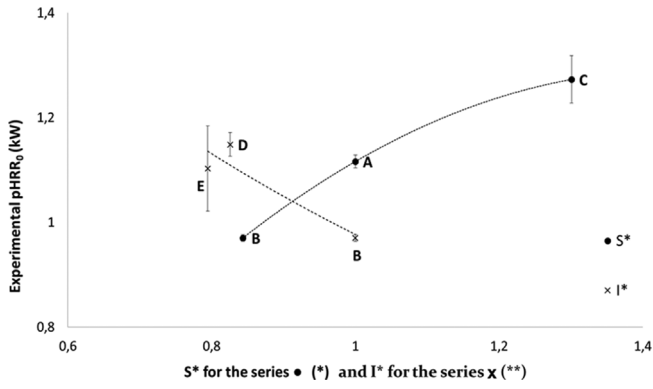


Fig. 8. Influence of the sheath thickness and the insulation mass on $pHRR_0$. (*) the data points for the series S^* , cables A, B and C are tested in configuration 6S1 at 50 kW/m^2 (where $HF^* = 1$; $N^* = 1$; $d^* = 1$; $I^* = 1$). (**) the data points for the series I^* , cables B, D and E are tested in configuration 6S1 at 50 kW/m^2 (where $HF^* = 1$; $N^* = 1$; $d^* = 1$; $S^* = 0,87$ for B or $S^* = 0,91$ for D or $S^* = 0,91$ for E)

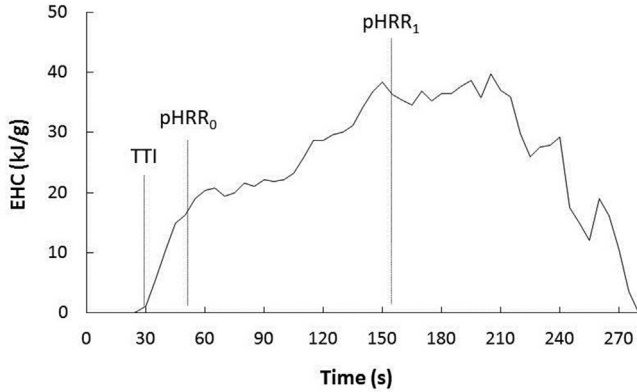


Fig. 9. Effective heat of combustion for reference test A_6S1_HF50.

observed the same phenomenon [3,32,33]. Therefore the influence of PE insulation on $pHRR_0$ shall be explained by an indirect effect: PE insulation absorbs a fraction of heat slowing down the heating of the sheath.

Density of cables has an influence on $pHRR_0$ (and also $pHRR_1$, see below). Higher is the density, lower are the peaks of heat release rate (Fig. 10). This is in qualitative agreement with our previous work on large halogen-free cables [11]. Indeed, in this work, when spacing increases (i.e. when density of cables decreases), the two peaks of heat release rate increase. This can be assigned to the increase of the exposed surface when cables are positioned in loose layout. In tight layout, one cable is partially protected by neighbored cables (Fig. 11). It is likely that spacing between cables may affect not only the radiative exposure but also the fluid dynamics around the sample. Hence the diffusion of heated air between cables may create turbulent convection and therefore modify the formation of the combustible mixture at the cable surface. The fuel concentration has a direct effect on the development of the flame and thus on HRR.

Note also that when spacing is the highest (3S4 samples), $pHRR_0$ does not increase anymore but decreases (Fig. 10). This may be assigned to a "side effect" (Fig. 12). Indeed, cables located in extreme position in this configuration are partly protected by the edges of the sample holder. Therefore the decomposition is slowed down and $pHRR_0$ decreases.

Another interesting point concerns the number of cables. Considering that the heat release rate of cables is additive, the $pHRR_0$ (and in fact, the whole HRR curve) should be equal to the $pHRR_0$ for one cable times the number of cables. It is not the case: when the

number of cables increases from 3 to 12, the $pHRR_0$ increases only by a factor 2 (Fig. 10). There are two possible explanations. The first one is only an artefact due to test conditions. Indeed, the spark igniter shades the cables located just below. Therefore the heating of these cables is slightly slowed down. If the cables do not ignite all in the same time, their respective HRR curve and especially $pHRR_0$ are slightly shifted. Experimental $pHRR_0$ is then lower than expected from a linear rule of mixtures.

Another explanation is that cables can be protected by the neighbored cables, as explained in Fig. 13. The cables located at the ends of the layout are more exposed than the cables located at the center. Moreover, for 12 cables, the two cables at the ends of the layout are also protected by the edges of the sample holder. This may explain why $pHRR_0$ is lower than expected, especially when 12 cables are burnt.

3.3. Influence of test parameters on $pHRR_1$

Fig. 14 shows the correlation between experimental and predicted $pHRR_1$ calculated according to equation (9). The R^2 coefficient is slightly lower than for TTI, $pHRR_0$ and Δt , but is considered satisfying.

$$pHRR_1 = 2,19 [HF^{*0,81}, N^{*1,14}, d^{*-0,2}, S^{*-1}, I^{*0,94}] \quad (9)$$

It appears that only the heat flux and the cable properties are influent.

Concerning the PE insulation, the influence is notable because $pHRR_1$ occurs when insulation is degrading. Higher is the amount of PE (remember that this component is not flame retarded), higher is the $pHRR_1$. On the contrary sheath thickness has a reverse effect on $pHRR_1$ (Fig. 15). Mineral layer accumulates during the decomposition of sheath (EVA and PE are pyrolyzed, while ATH releases water and alumina remains in the condensed phase). This layer is able to slow down heat transfer from the flame to the underlying material and to reradiate a part of the heat flux. Higher is the sheath thickness, higher is the protective mineral layer thickness and more limited is the heat transfer. As developed by Braun et al., this protective jacket comes to burst, exposing the insulation to the heat flux [3].

Of course, heat flux has also a positive effect on $pHRR_1$. Higher is HF, higher is $pHRR_1$.

3.4. Influence of test parameters on Δt

Fig. 16 shows the correlation between experimental and predicted Δt calculated according to equation (10).

$$\Delta t = 89,16 [HF^{*-0,59}, N^{*0,39}, d^{*0,8}, S^{*1,06}, I^{*-0,21}] \quad (10)$$

Four parameters are influencing Δt : heat flux, number of cables,

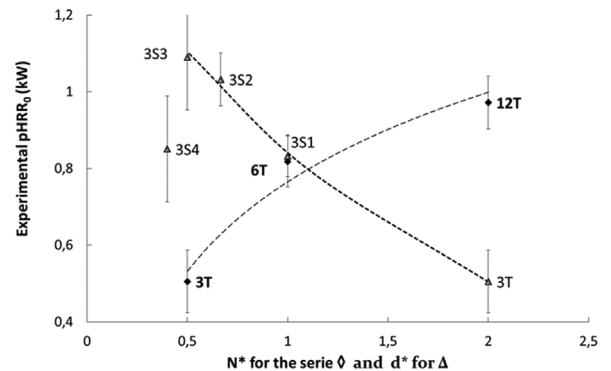


Fig. 10. Influence of the number of cables and their density on $pHRR_0$. (*) the data points for the series N^* , cable A is tested in configurations 12T, 6T and 3T at 50 kW/m^2 (where $HF^* = 1$; $d^* = 2$; $S^* = 1$; $I^* = 1$). (**) the data points for the series d^* , cable A is tested in configuration 3T, 3S1, 3S2, 3S3 and 3S4 at 50 kW/m^2 (where $HF^* = 1$; $N^* = 0,5$; $S^* = 1$; $I^* = 1$)

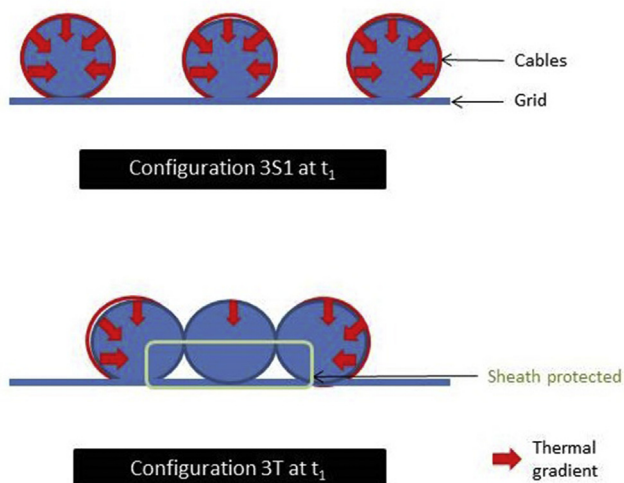


Fig. 11. Scheme illustrating the protective effect of neighbored cables in tight layout.

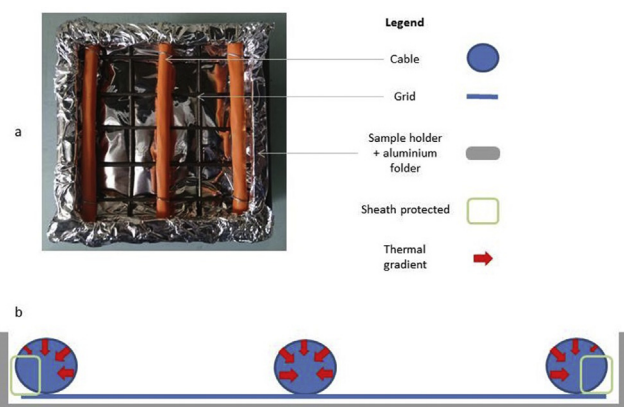


Fig. 12. Configuration 3S4D – a. Picture of cables in sample holder – b. cross-section illustrating the protection from the edges of sample holder.

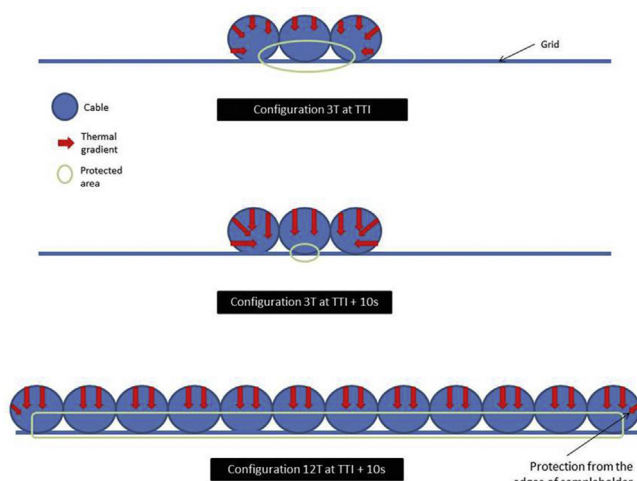


Fig. 13. Scheme illustrating the heat flux according to number of cables in tight layout.

density of cables and sheath thickness. The two last parameters are the most influent. Higher is the sheath thickness, longer is the time needed to degrade the sheath before starting degrading the PE insulation (remember that $pHRR_1$ corresponds to PE pyrolysis) (Fig. 17).

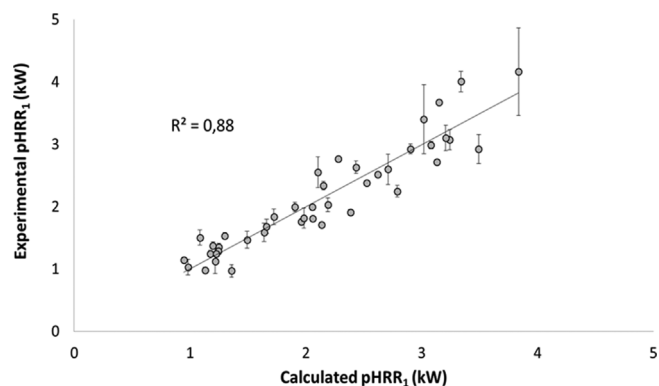


Fig. 14. Experimental versus calculated $pHRR_1$.

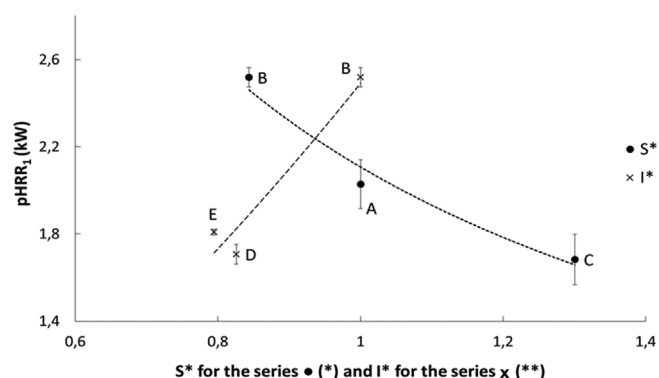


Fig. 15. Influence of the sheath thickness and the insulation mass on $pHRR_1$. (*) the data points for the series S^* , cables A, B and C are tested in configuration 6S1 at 50 kW/m^2 (where $HF^* = 1$; $N^* = 1$; $d^* = 1$; $I^* = 1$) (**) the data points for the series I^* , cables B, D and E are tested in configuration 6S1 at 50 kW/m^2 (where $HF^* = 1$; $N^* = 1$; $d^* = 1$; $S^* = 0,87$ for B or $S^* = 0,91$ for D or and $S^* = 0,91$ for E)

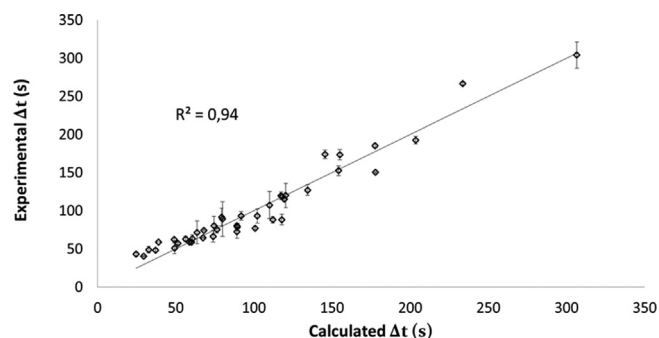


Fig. 16. Experimental versus calculated Δt .

As already explained, when the layout of cables is loose (low d value), the exposed surface increases and then the decomposition is faster. Therefore $pHRR_1$ is reached after a shorter period and Δt decreases. This was also observed for larger halogen-free cables for which the spacing between cables was studied in cone calorimeter [11].

Obviously, higher is the heat flux, faster is the decomposition, and Δt decreases too. The effect of the number of cables is less obvious. It may be due to a correlation with density of cables to some extent. Indeed, when the number of cables is large, their 'density' is also higher. In the case of 12 cables, the only configuration is tight, instead of the case of 3 cables that can be organised in loose configurations. The simulated importance of the number of cables may be an artefact of this experimental setting. So the decomposition is faster for 3 cables, and the $pHRR_1$ is reached sooner. But this parameter has only a moderate influence in comparison to sheath thickness.

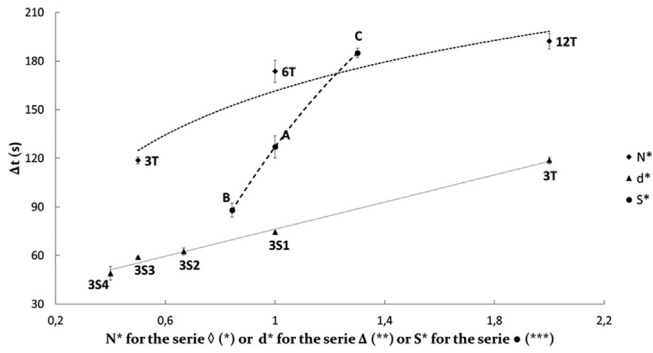


Fig. 17. Influence of the number of cables, the density and the sheath thickness on Δt .

(*) the data points for the series N^* , cable A is tested in configurations 12T, 6T and 3T at 50 kW/m^2 (where $HF^* = 1$; $d^* = 2$; $S^* = 1$; $I^* = 1$).

(**) the data points for the series d^* , cable A is tested in configuration 3T, 3S1, 3S2, 3S3 and 3S4 at 50 kW/m^2 (where $HF^* = 1$; $N^* = 0.5$; $S^* = 1$; $I^* = 1$).

(***) the data points for the series S^* , cables A, B and C are tested in configuration 6S1 at $HF^* = 0.5$; $N^* = 1$; $d^* = 1$; $I^* = 1$.

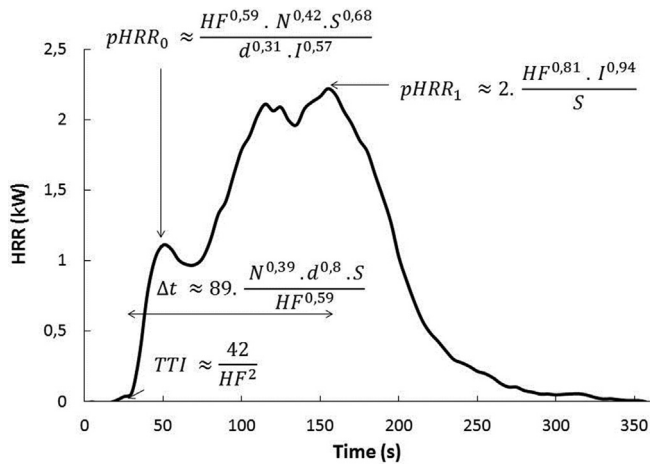


Fig. 18. Prediction of the cone calorimeter test for cables A. B. C. D. and E.

3.5. Some additional remarks

Sheath thickness has a significant influence on 3 among 4 features, namely $pHRR_0$, $pHRR_1$ and Δt . Only TTI does not appear to be influenced by sheath thickness. On the contrary, PE insulation has a negligible influence on TTI and Δt , a moderate one on $pHRR_0$ but a strong influence on $pHRR_1$. This result highlights the predominant role of sheath with respect to decomposition rate. This is an expected result since sheath is the first layer undergoing heat flux in case of fire. But it means that a huge improvement of flame retardancy can hardly be obtained by changing only the inner cable structure.

Note also that the whole cables are fully burning in all cases. No heat flux threshold was observed, as in the previous work of Meinier et al. [11]. Of course, this may be assigned to the low sheath thickness of the cables studied in the present work. This highlights that the sheath is unable to sufficiently slow down the heat transfer to avoid the pyrolysis of the inner parts. This evidences that these relatively thinner cables are much more hazardous than bigger ones despite a lower fuel load per length unit.

Fig. 18 summarizes the main findings of this work. The whole HRR curve can be described by part through the values of TTI, $pHRR_0$, $pHRR_1$ and Δt . These values are the main properties accounting for decomposition rate of the cables. While the cables are fully burning, THR may be also predicted directly from the composition and the

number of cables (note that the THR is an unchanged parameter). The effective heat of combustion or the residue content are also unchanged because the burning is complete (no flame inhibition phenomenon is expected).

4. Conclusion

HRR curves of halogen-free cables tested in various conditions were described using four main features: TTI, first and main $pHRR$ and Δt (delay between TTI and $pHRR_1$). These features were successfully related to experimental and material parameters using power laws. Five parameters were taken into account, namely heat flux, number and density of cables, sheath thickness, and insulation weight. This fitting allows not only to predict the fire performance of such cables in cone calorimeter but also to highlight the respective role of each parameter investigated through the exponent of the power law.

Depending on the features, one to four parameters have to be considered in the power law to correctly predict experimental data. Heat flux influences all these features and even is the only influent parameter on TTI. Therefore it appears difficult to delay the ignition by small changes in the cable structure. The number of cables and their layout (tight or loose when spacing increases) have an effect on $pHRR_0$ and the delay between TTI and $pHRR_1$. By increasing the number of cables, the fuel amount is more important, so the first peak of heat release rate increases. Nevertheless the HRR curve is not fully proportional to the number of cables. The increase of spacing between cables enhances the exposed surface, accelerating the pyrolysis of the sheath and the insulation.

The results also highlight the major role of the sheath (especially, in this study, the sheath thickness) on the HRR curve in comparison to other cable structure parameters. PE insulation mass has a huge effect on $pHRR_1$ because this peak occurs when PE is degrading. But the two $pHRR$ s and the delay between TTI and $pHRR_1$ are strongly influenced by the sheath thickness. Indeed, the sheath is directly exposed to heat flux and contributes to the early heat release. But gradually as the cable burns, alumina from ATH decomposition accumulates at the top of the cable and forms a protective mineral layer able to slowdown the heat transfer from the flame to the underlying material.

The equations proposed to fit experimental data are only suitable for a narrow range of cables. Further work will investigate the extension of our approach to other cables and parameters as for the copper, material of huge importance in the fire behaviour of cables. No quantitative influence of this parameter can be discussed with the set of cables tested in this article since they contain almost the same amount of copper (difference of only 11% between the cables).

We hope this approach provides a guideline for cable engineers to design the cable structure in order to improve its fire performance in cone calorimeter. Of course, this phenomenological model is only suitable for a narrow range of cable properties. Further investigation will attempt to extend it to a larger set of cable properties including sheath material.

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Appendix A. Supplementary data

Supplementary data related to this article can be found at <http://dx.doi.org/10.1016/j.firesaf.2018.05.001>.

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